# SYNTHESIS AND CHARACTERIZATION OF TRANSITION ALUMINAS FROM RECYCLED SCRAP ALUMINIUM

Síntesis y caracterización de alúminas de transición a partir de desechos de aluminio reciclado

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## ABSTRACT

The aim of this study was to develop an alternative methodology for the synthesis of transition aluminas, in order to reduce ecological costs by using recycled metal scrap as raw material (cans of soft drinks) and generate a product with high added value. The synthesis technique employed yielded a precursor comprised of 55.4 % of bayerite, 41.2 % of boehmite, and ammonium salt, according the characterization performed with X-ray diffraction and quantification by the Rietveld method. The ammonium chloride salt present is not relevant for the process, since given its solubility in water, it could be eliminated by successive washing. Scanning electron microscopy evaluations showed the presence of agglomerates of particles between 50 and 300  $\mu$ m. A bimodal grain sizes distribution was detected during the laser granulometric test. Thermogravimetric analysis of the precursor indicated a 40.6 % total weight loss at 1000 °C. The heat treatments at 350 and 750 °C of precipitates for 1, 2 and 4 h, produced various transition aluminas ( $\gamma$ ,  $\eta$ ,  $\theta$ ), which are products where value has been added and might have a potential use as binders in monolithic products, catalyst support, or additives for puzzolanic materials, among others.

Palabras clave: latas, aglutinante, materia prima.

## RESUMEN

El objetivo de este estudio fue desarrollar una metodología alterna para sintetizar alúminas de transición, partiendo de aluminio reciclado como materia prima (latas de bebidas gaseosas), a fin de disminuir los efectos ecológicos de este tipo de desecho y generar un producto de alto valor agregado. Con el método de síntesis implementado se obtiene un precursor conformado en un 55.4 % por bayerita, 41.2 % por bohemita y el resto por sal de amonio, de acuerdo con los estudios de rayos X realizados y la cuantificación por el método de Rietveld. La sal cloruro de amonio generada no es relevante para el proceso manejado, ya que su alta solubildad en agua permite eliminarla por lavados sucesivos. Estudios realizados por microscopia electrónica de barrido muestran la presencia de partículas aglomeradas con tamaños de 50 a 300 µm. Utilizando ensayos de granulometría laser, se determinó una distribución bimodal del

tamaño de grano. El análisis térmico indicó una pérdida de masa del 40.6 % en peso respecto de la muestra inicial del precursor al llevar la muestra a temperaturas cercana a los 1000 °C. Tratamientos térmicos a 350 y 750 °C realizados al precipitado obtenido, manteniendo la temperatura durante 1, 2 y 4 h, permitieron obtener varias alúminas de transición ( $\gamma$ ,  $\eta$ ,  $\theta$ ), que son productos con valor agregado que tienen usos potenciales como aglutinantes para refractarios monolíticos, soportes catalíticos o aditivos como materiales puzolánicos.

### **INTRODUCTION**

As a technological material, alumina represents a great opportunity, because its properties allow very diverse applications that can range from the food and pharma industry to the chemical and electronic industry. Alumina can undergo different polymorphic transformations depending on the conditions in which these transformations are carried out (West 2014): thermal and via precursors, which allow obtaining different crystalline phases called transition aluminas (Levin and Brandon 1998). Three large types of alumina are known industrially: metallurgical grade, ceramic grade and transition aluminas. This last group, due to its multiple crystallographic and allotropic forms, presents the greatest number of uses and applications (West 2014). These aluminas can be used as catalyst support in combination with other activated transition aluminas (De Souza et al. 2000), as well as cementitious material of interest for its use as high temperature refractory cement (Lee and Moore 1998).

The aim of this work is to determine a technological path that, starting with recycled aluminium in Venezuela (Vitalis 2015), allows obtaining transitional aluminas (Mahinroosta and Allahverdi 2018). An important point is the handling of the raw material (Gonzalo 2008) to be used in this process, which follows the global recycling trend instead of continuing with the degradation of the different ecological systems from which the different precursors can be obtained (Schlesinger 2007).

We propose the use of soft-drink cans (Adans et al. 2016), which have a high potential in terms of reducing, recycling and reusing (RRR). In general, the vast majority of materials, especially those of metallic type, can be recycled once their useful life is over, thus giving way to materials of the same nature or with some variation to satisfy the needs of the market without having to resort to the sources of the metal. Such is the case of aluminium for soft-drink cans, whose postconsumer deposits (used beverage cans, UBC) are of particular interest for the present study. According to the Venezuelan regulation COVENIN 2352-86, the

aluminium content in these deposits should be in the order of 97 % (Iesmat 2015). These products represent a source of aluminium of relatively high purity with a high potential for recycling or reuse (COVENIN 1986). In general, the vast majority of materials, especially those of metallic type, can be recycled once their useful life is over, giving way to materials of the same nature or with some variation to meet the needs of the market without resorting to metal sources (Meshram and Kumar 2018). However, since the production levels of transition aluminas are very limited (if not inexistent) in Venezuela, obtaining materials of this nature may represent an alternative both for the development of new technologies and for companies that seek to stock up on this type of material or any other that may act as a precursor. In summary, we propose a method of reusing metallic aluminium from waste to obtain ceramics material with added value.

## **MATERIALS AND METHODS**

The experimental procedure included four steps (Fig. 1):

- Synthesis of the precursor through precipitation in aqueous media at low temperature (25 °C, ambient temperature); heating of cans at 500 °C for 45 min (López et al. 2018); dissolution in HCl; pH adjustment with ammonium hydroxide (Sharma 2003), and aging precipitates (De Souza 1990, Ahmedzeki et al. 2017).
- Characterization of the precursor by X-ray diffraction (XRD): 10°-90° (0.02°/seg, CuKα), 35 KV, 25 mA; scanning electron microscopy/energy dispersive spectroscopy (SEM/EDS): secondary electrons, and particle size distribution (PSD): 0.02-2000 μm.
- 3. Thermogravimetric analysis (TGA) and thermogravimetric differential analysis (TDA), thermal treatment of the precursor in order to achieve transition aluminas.
- 4. Characterization of the resulting products.



SEM/EDS: Scanning Electron Microscopy/Energy Dispersive Spectroscopy TGA/TDA: Thermogravimetric Analysis/Thermogravimetric Differential Analysis

Fig 1. Flowchart of the experimental procedure.

#### **RESULTS AND DISCUSSION**

Chemical composition analyses of the raw material (aluminium cans) and the precursor (precipitated material) were performed by SEM/EDS. The results (**Table I**) were as expected for both materials. Chlorine (Cl) was detected in the precipitated precursor due to acid media dissolution with HCl and pH adjustment with ammonium hydroxide (NH<sub>4</sub>OH), as well as some reaction products according to the following formula:

$$2Al_{(s)} + 8HCl_{(aq)} + 2NH_4(OH)_{(aq)} \rightarrow 2AlCl_{3(aq)} + 2NH_4Cl_{(aq)} + 3H_{2(g)} + 2H_2O(l)$$
(1)

**TABLE I.** CHEMICAL COMPOSITION OF ALUMINUM<br/>SCRAP AND PRECIPITATED PRECURSOR<br/>BY SCANNING ELECTRON MICROSCOPY/<br/>ENERGY DISPERSIVE SPECTROSCOPY.

Element (wt %)	Raw material	Precursor
Mg	2.33	_
Al	96.24	87.76
Mn	0.87	—
Fe	0.57	—
Cl	—	12.24

It is relevant to note that no metallic elements (like Fe or Mn) were observed in the precursor, indicating that the controlled precipitation process could allow the synthesis of materials free of contaminants.

The precursor was characterized using different techniques: XRD, PSD and morphological assessment with SEM. Boehmite ( $\gamma$ -AlOOH) and bayerite ( $\alpha$ -Al(OH)<sub>3</sub>) were detected by XRD (**Fig. 2**). Both compounds are precursors phases of transition aluminas according to the sequences of phase transformations toward the stable  $\alpha$ -phase reported in literature (West 2014). Percentages of detected phases were estimated with the Rietveld technique and pseudo-Voigt adjustment (Young 2002).

The composition of the precipitated precursor was 55.4 % of bayerite, 41.2 % of boehmite and 3.4 % of ammonium salt. The PSD of the precursor (**Fig. 3**) indicates a bimodal distribution with two distinctive particle sizes, 68 and 500  $\mu$ m, respectively (Iesmat 2015). The SEM evaluation (**Fig. 4**) revealed agglomerates with particle size ranging from 50 to 300  $\mu$ m, which confirmed the PSD performed with laser granulometer. Also, particles with sizes around 1  $\mu$ m were observed.

The thermal evolution of the precursor was studied through typical DTA/TGA methodologies (Smykatz-Kloss 1974). The dehydration appears to start at 106 °C (**Fig. 5a**), indicated by



Fig. 2. X-ray diffraction of the precipitated precursor.



Fig. 3. Particle size distribution of the precursor.

the endotherm peak, and continues up to 145 °C, probably because the small capillarity of the gelatinous precursor slowed down the water loss through the material. This step accounts for 8 % of the mass loss. A sharp exothermic peak appears at 225 °C, which represents energy release during the transformation phase from bayerite to n-alumina (Sato 1962). Another step occurres between two endothermic peaks at 260 and 360 °C, which may be attributed to two events: elimination of residual hydroxyls and ammonium chloride decomposition. The exotherm that appears at 490 °C corresponds to the transformation of boehmite into  $\gamma$ -alumina (Alphonse and Courty 2005). Thermal evolution occurring between 190 and 750 °C, approximately, account for 30 % of mass loss (Fig. 5b).

Discrepancies between TDA and TGA curves may indicate that the change in enthalpy is not directly proportional to the rate of mass loss, which is normally encountered in complex reactions. However, in the present study, all the events observed during thermal evolution analysis were confirmed with Xray diffractograms at various temperatures of the precursor (**Fig. 6**).

Since transition aluminas could be prepared by calcining aluminium hydroxides, thermal treatment of the precursor was conducted at 350 and 750 °C at a rate of 10 °C/min for 1 h and 4 h (Dwivedi 1985). The obtained product was characterized by XRD. Different kinds of transition alumina were obtained after the thermal treatment of the precursor:  $\eta$ -Al<sub>2</sub>O<sub>3</sub> (**Fig. 7a**) and x-Al<sub>2</sub>O<sub>3</sub>  $\Theta$ -Al<sub>2</sub>O<sub>3</sub> (**Fig. 7b**).

In order to detect possible hydraulic activity of the obtained transition aluminas, heat-treated samples of synthesized product (at 350 and 750 °C) were subjected to hydration with distilled water for 168 h. Then the samples were washed with ethanol and prepared with gold for the observation in SEM model FEi Inspect F50. The comparison of morphological features (**Fig. 8a, b**) (heat-treated samples at 350 °C) reveals morphological changes of the transition aluminas after hydration. These transformations are correlated with those studied by Lefévre et al. 2002 and Sato 2007, who characterized this type of transformation for periods of 4 days, observing a transient amorphous hydrated phase, followed by an increase in bayerite concentration, which stabilizes after about two months. Thermodynamical calculations predict the hydration reaction of  $\gamma$ -alumina leading to a more stable phase (bayerite, gibbsite, or boehmite), since the surface reactivity and sorption properties of solids are factors controlling the transport of elements in water. This could be an indication of potential hydraulic activity due to the formation of new phases. In contrast, comparison of heat-treated samples at 750 °C and 168 h (Fig. 8c, d) with and without hydration, did not show any relevant difference in morphological features; thus, apparently this material does not present any hydraulic activity, at least under this conditions

Nanometric particles smaller than 100 nm (**Fig. 9**) were observed in the synthesized transition aluminas heat-treated at 350 °C. This shows that the synthesis technique could yield micro- and nanometric alumina particles with potential conditions to be used in the binding systems of monolithic refractories. However, some parameters needs to be adjusted in future studies in order to improve the results of this preliminary work.



Fig. 4. Morphological evaluation of precursor by scanning electron microscopy.



Fig. 5. Thermal evolution of the precursor (a) by thermogravimetric differential analysis (TDA) and derivate thermogravimetric differential analysis (DTDA); (b) by thermogravimetric analysis.



Fig 6. X-ray diffractograms of the thermal evolution of the precursor.



Fig. 7. X-ray diffractograms of synthetized transition alumina at (a) 350 °C for 4 h; (b) 750 °C for 4 h.



Fig. 8. Photomicrographs of transition aluminas at different conditions: (a) heat-treated at 350 °C without hydration, (b) heat-treated at 350 °C and hydrated for 168 h, (c) heat-treated at 750 °C without hydration, (d) heat-treated at 750 °C and hydrated for 168 h.



Fig. 9. Photomicrographs of transition aluminas heat-treated at 350 °C and hydrated for 168 h: (a) 120.000X and (b) 240.000X.

# CONCLUSIONS

It is possible to synthesize transition aluminas  $(\gamma, \eta, \theta)$  from aluminium scrap by using controlled conditions of a wet-chemical route. The presence of the  $\rho$ -Al<sub>2</sub>0<sub>3</sub> phase is not ruled out, due to the amorphous region observed in the diffraction pattern of the sample.

According to the synthesis method, it is possible to obtain transition aluminas in particularly interesting combinations for their application as catalyst supports, activated aluminas or pozzolanic additives for cement. In the near future, these materials could be potential candidates for binding systems in monolithic refractories. Further studies will be conducted to adjust variables in the methodology, for example, the application of washes to remove ammonium chloride.

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